

SFSA Digital Innovative Design for Reliable Casting Performance (DID)

SAE FD&E Spring Meeting

April 15, 2020 – virtual meeting



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David Poweleit

Steel Founders' Society of America (SFSA)





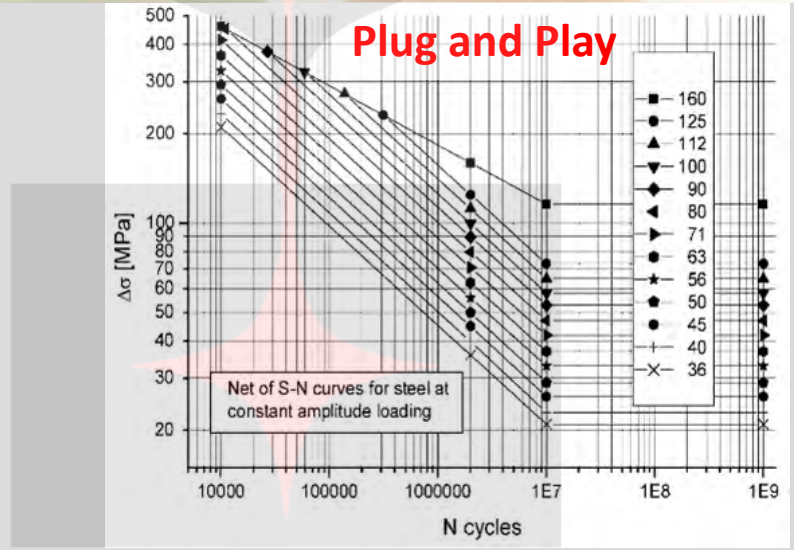
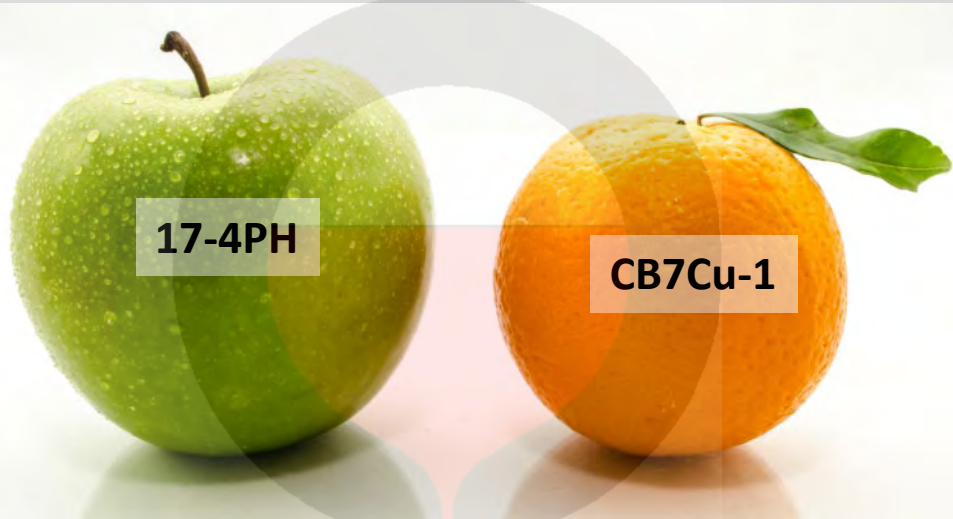
Steel Founders' Society of America (SFSA)

- Our organization
 - Not for profit technical society founded in 1902
 - Goal is advance the steel casting industry
- Our members
 - Are all steel casting producers
 - Have a culture of collaboration and innovation
- Our industry
 - ~1M tons produced
 - About 9M tons worldwide
 - Major markets: railroad, mining, construction, trucks, pumps/valves, oil and gas, energy, industrial equipment, and military



EH tapping at Bradken-Atchison

Change the way we think!





Design, Manufacturability & Reliability

- What is DID?

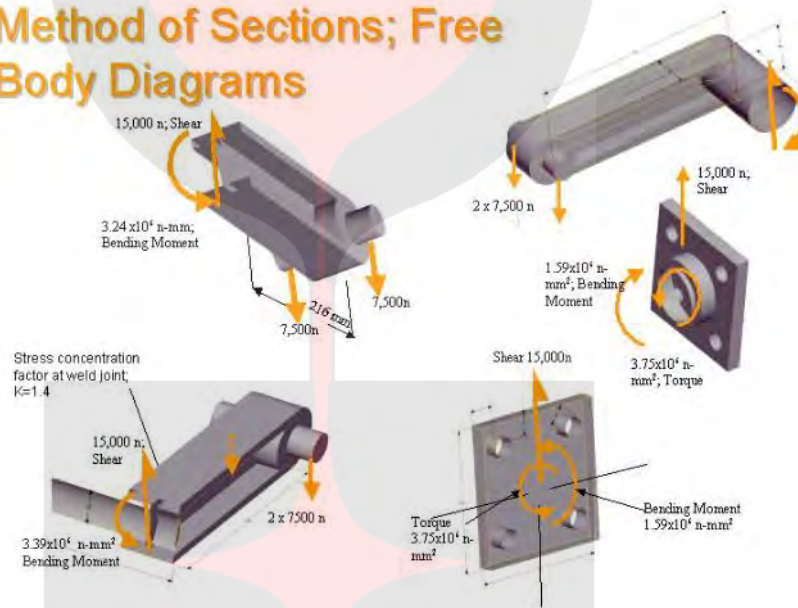
Not
IP



Digital Innovative Design

for Reliable Casting Performance

Method of Sections; Free Body Diagrams

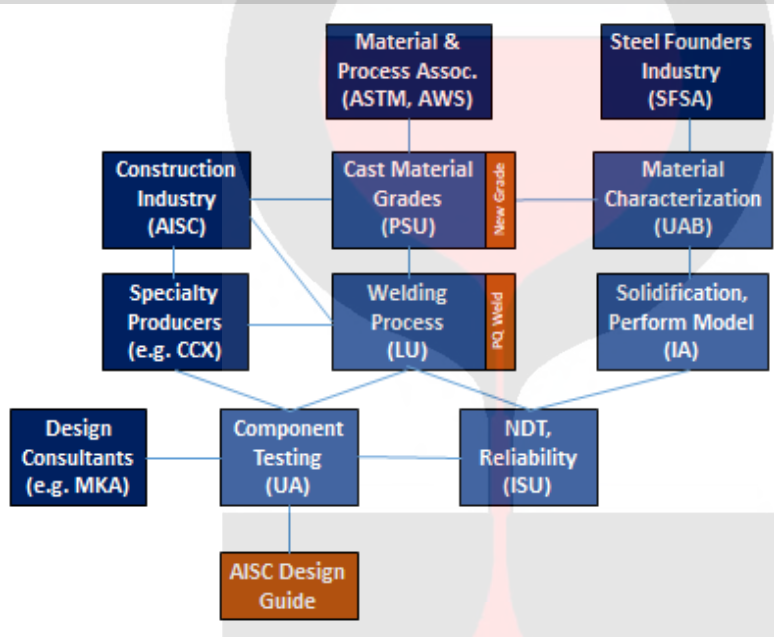


*An engineered approach to steel casting performance
For a multitude of partners and purposes*



Collaborative Research

Example – castings for building construction



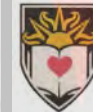
Government

- Defense Logistics Agency (DLA)
- DOD

Industry/Consultants/Other Stakeholders

- SFSA Members
- Darrell Socie – BBM Plus
- OEM's/Partners – GD, Emerson, Magma, AISC, Deere and Cat

Academia

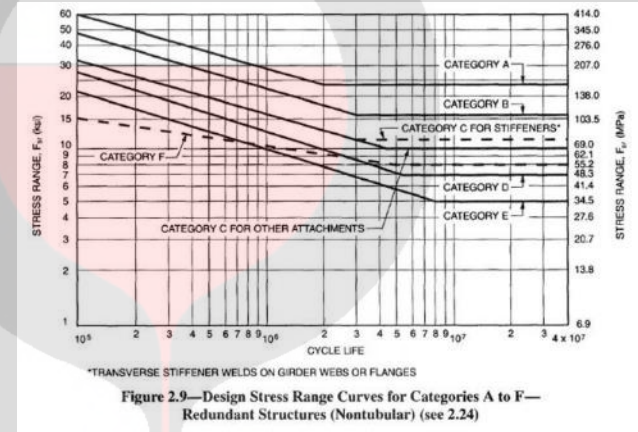




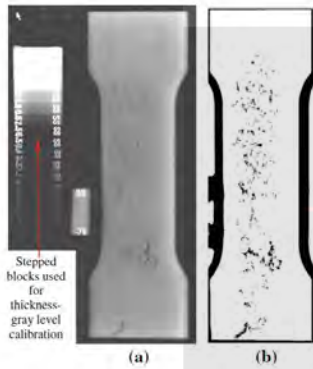
DID Design Methodology

- Codes based on design allowables
- Model-based Process & Performance Design (MP²D) – lower bound modeling for local properties

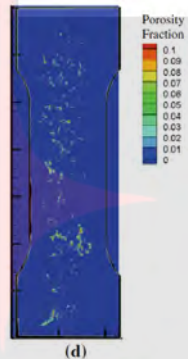
NDT strategy for economic and performance design – quantitative for performance NDT



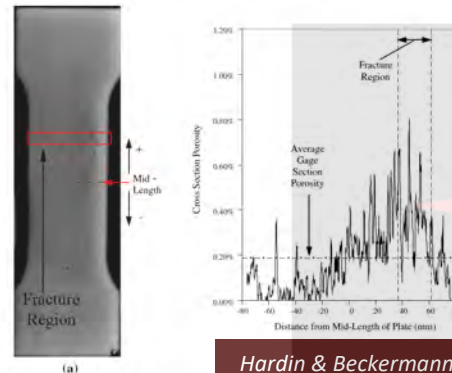
NDT Level



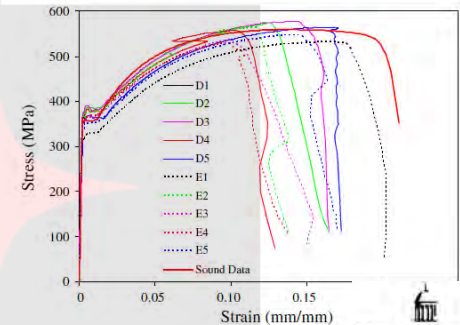
“Quality” Index



Key Quantitative Measures



Structural Performance

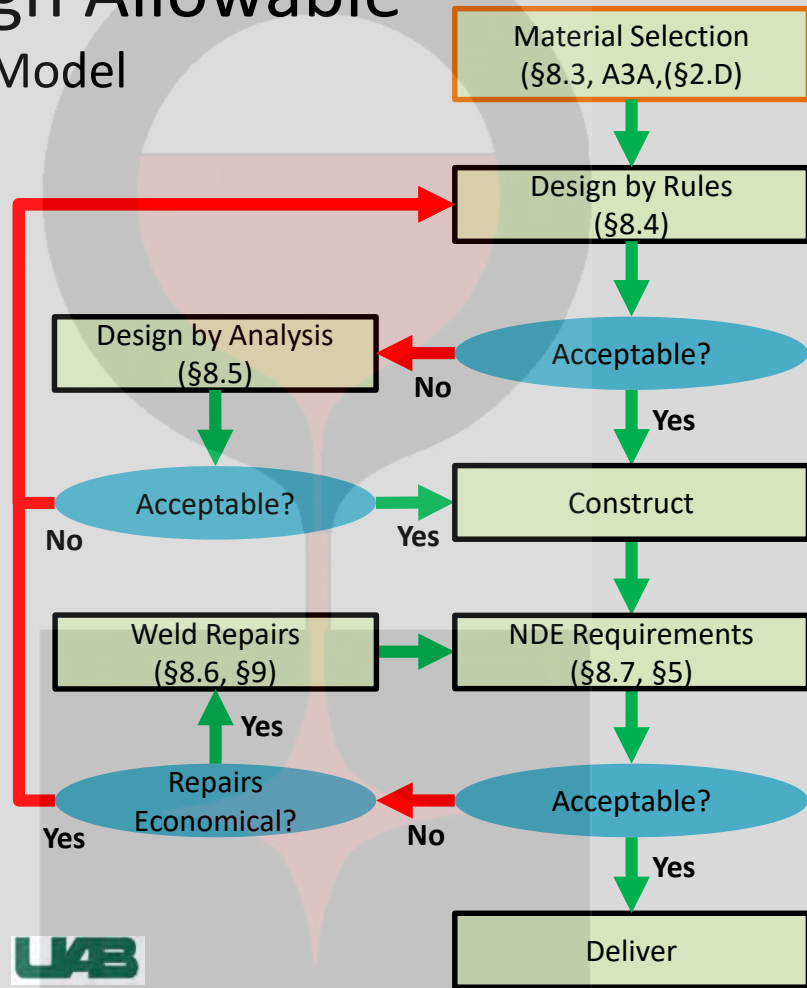




Code-based Design Allowable

ASME BPVC Model

- Section II for design allowables plus adopted ASTM standards, e.g. SA216
 - “ASME allowable” with NDT
 - ASTM A216 WCB 36 ksi min YS has allowable design stress of 20 ksi
 - 0.8 “ASME allowable” without NDT
 - ASTM A216 WCB 36 ksi min YS has allowable design stress of 16 ksi
- Section V Volumetric Methods SG
- Section VIII Div-1 & 2 for examination requirements/NDT
 - RT per ASTM E446 in critical sections - limits on porosity and shrinkage
 - MT per ASTM E125 - limits on linear indications, shrink, porosity, inclusions, etc.
 - PT - limits no linear indications > 1/4 in, no non-linear indications > 3/16 in
- Section IX for welding

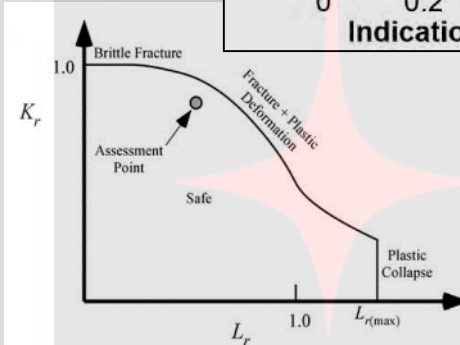
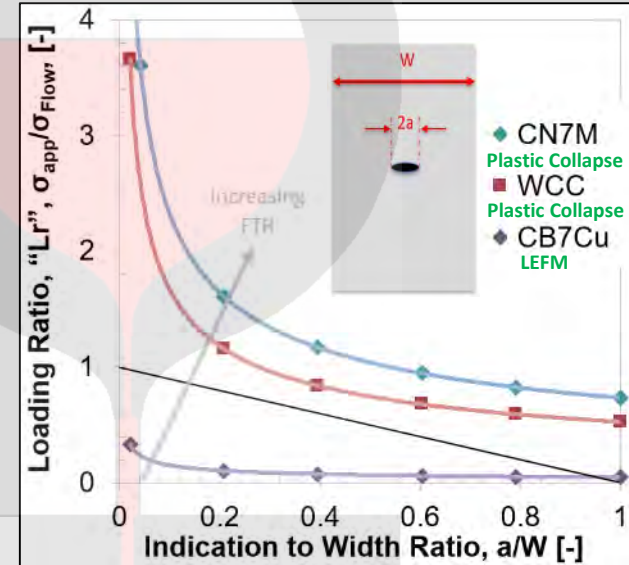
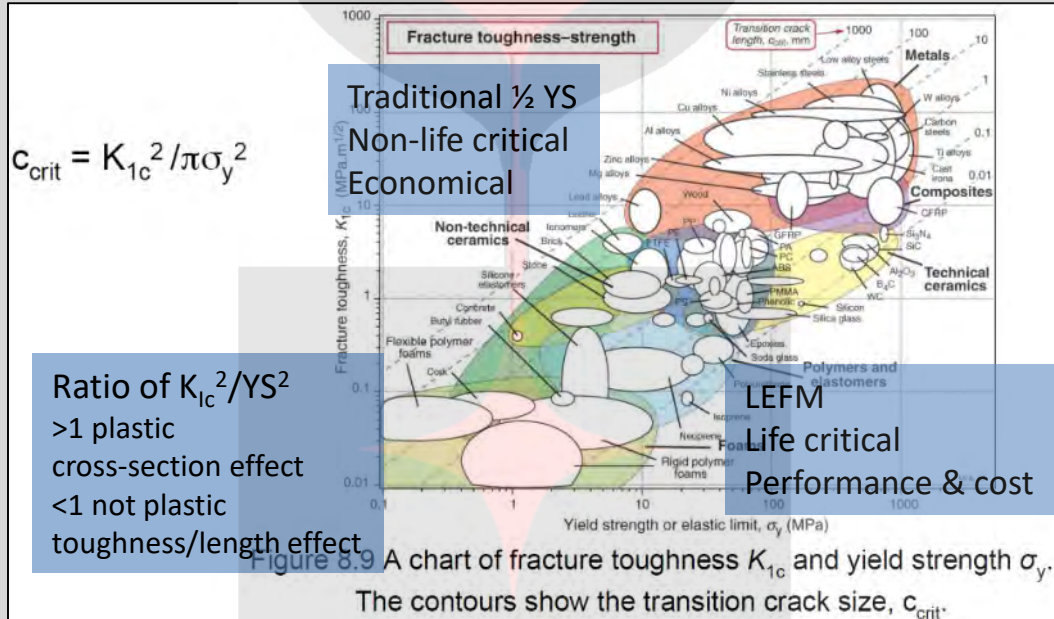




Fracture Toughness Ratio Effect on Limiting Load

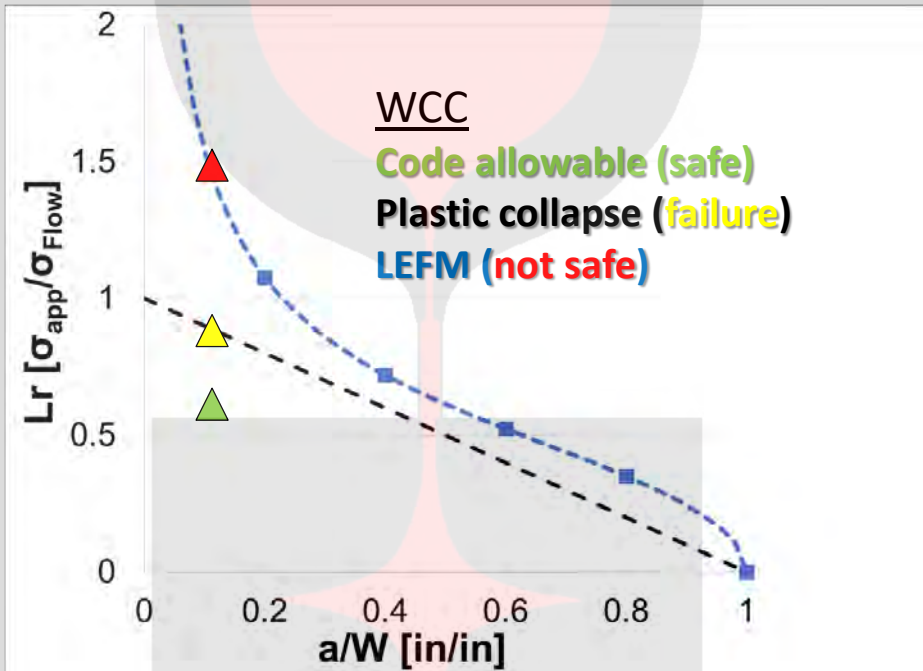
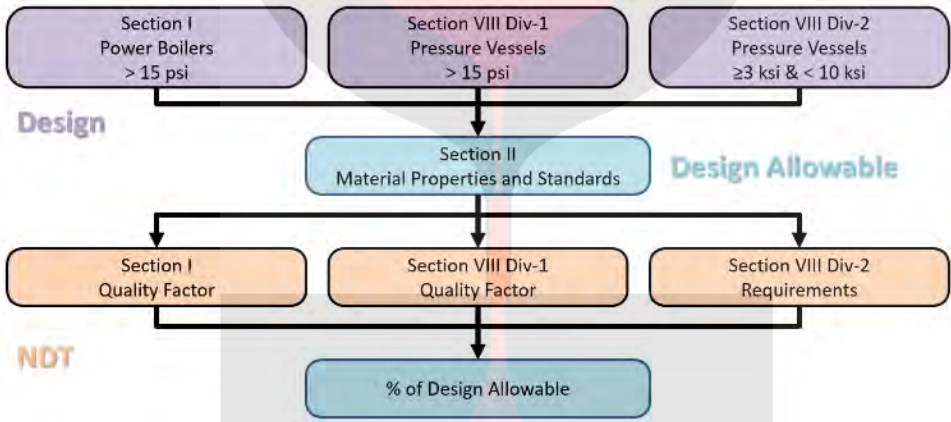
Brittle Failure (LEFM) v. Plastic Collapse

Performance controls: material, indication size, indication location (local loading)





Relationship to BPVC





Parametric Design Model and Sensitivity Analysis

| Load Type | Component Design | Largest Notch | Failure Criteria |
|--|---------------------------------------|--|--|
| static impact low-low fatigue (1,000) low fatigue (100,000) high fatigue (1,000,000) | Shape: bar, tube, "L" Size Load | Location: surface, internal Geometry: crack/notch, size, quantity/proximity, linear v. non-linear | YS $\frac{1}{4}$ YS $\frac{1}{2}$ YS $\frac{3}{4}$ YS ASME allowable 0.8 ASME allowable |

Analytical failure analysis with strain controlled fracture mechanics and LEFM.
Not developing crack growth or propagation theory.

Program will not be pursuing MMPDS but will leverage a similar statistical analysis

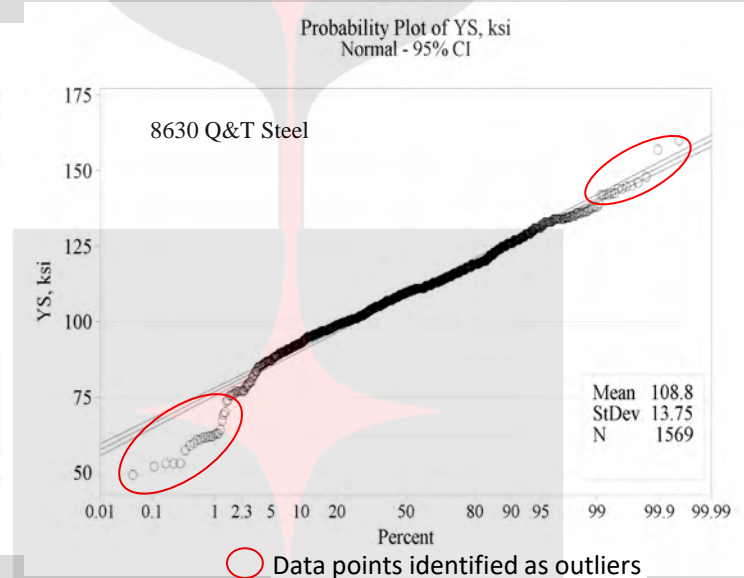
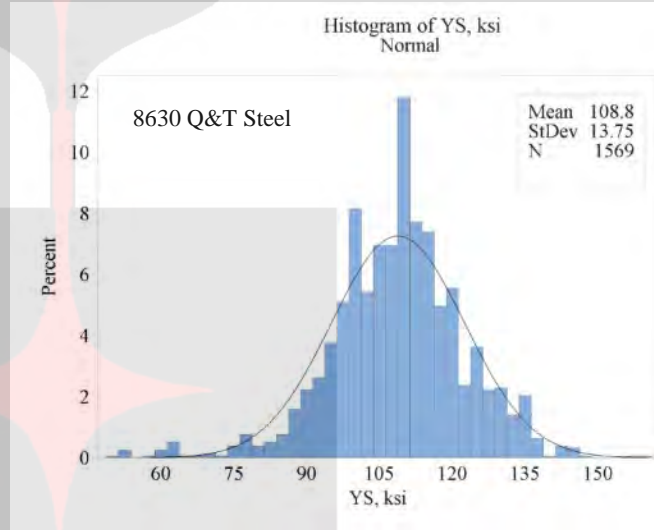


Lower Bound Mechanical Properties (8630)

Determined from SFSA Data

- Mechanical test data for yield and ultimate strengths, elongation and reduction of area have been analyzed for 10 alloys in ASTM A958 and A487.
- Data set contains over 7000 tensile test results.

Example Data for Normal Distribution, Histogram and Probability Plots of Yield Stress Data for 8630 Quenched and Tempered Cast Steel Data Collected from SFSA Members



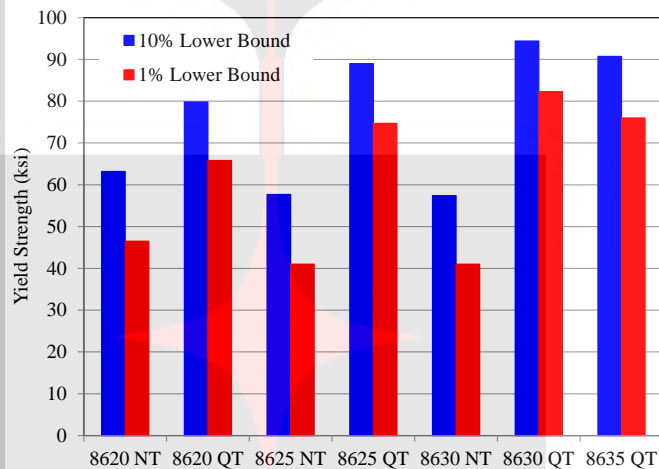


Example Lower Bound Properties (8630)

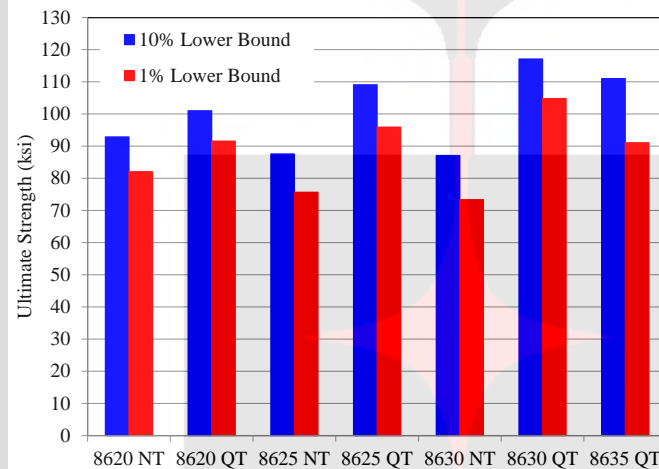
Calculated from SFSA Data

- Calculations made at the 1% and 10% levels, “A” and “B” allowables by MMPDS approach
- Data below is organized by ASTM A958 for seven 86xx alloys
- Results have also been analyzed for data organized by ASTM A487 for three alloys

Yield Strength



Ultimate Strength

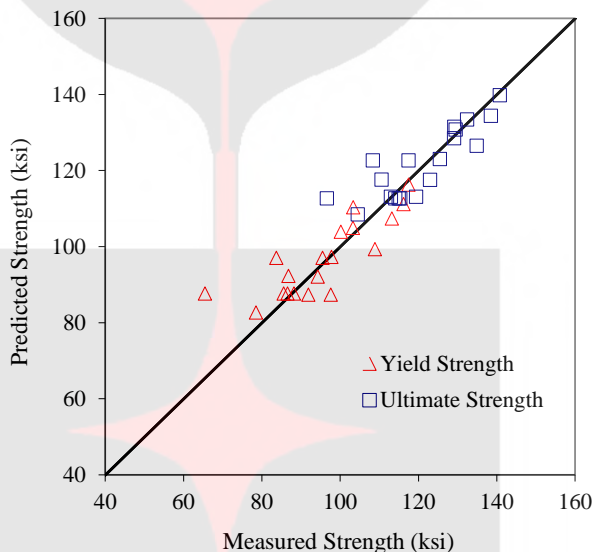




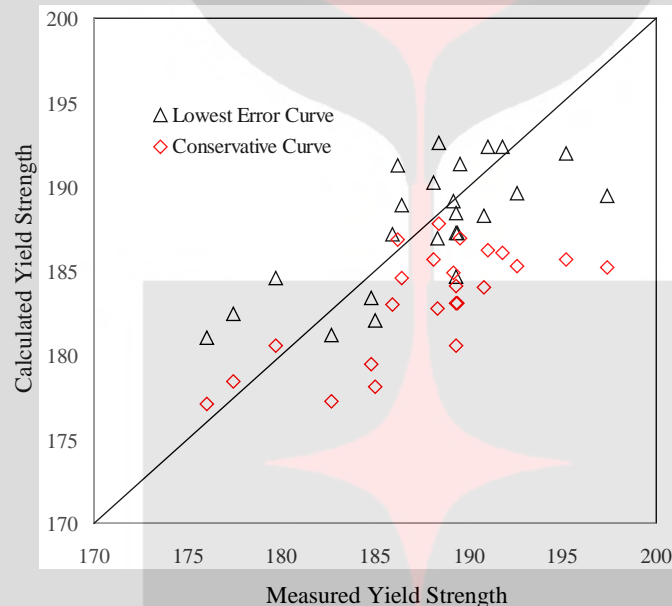
Solidification & MAGMAsteel Property Prediction

YS and UTS

8630 Q&T yield and ultimate strengths predicted from results of *MAGMAsteel* heat treatment model and additional variables such as cooling rates during quench vs. measurements

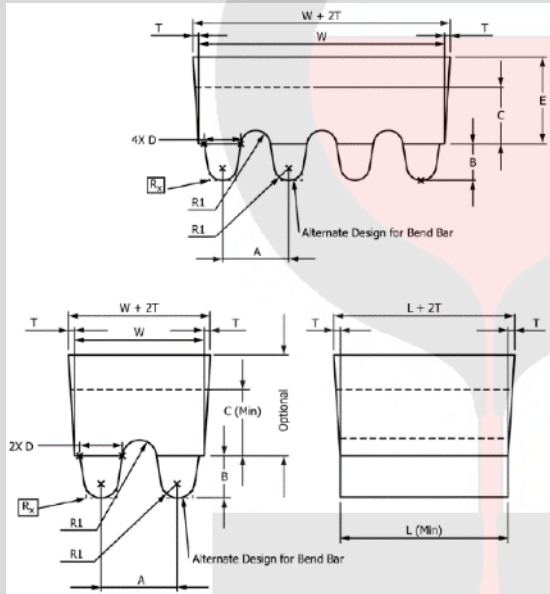


AF9628 Yield strength predicted from solidification cooling rates, lowest error and conservative lower bound curves vs. measurements



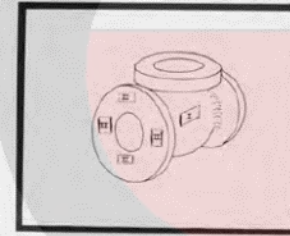


Casting v. Test Coupon Properties



Quality factors

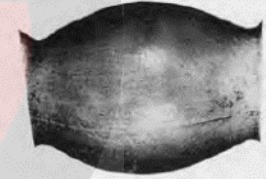
- Porosity
- Segregation
- Welding
- Inclusions
- Cooling rate
- Surface finish
- Others
 - Grain size
 - Embrittlement



TEST SPECIMEN LOCATIONS AND TYPES

TENSILE AND IMPACT DATA

| | I | II |
|-------------------------------|------|-----|
| Tensile (1000 PSI) | 73 | — |
| Yield (1000 PSI) | 43 | — |
| Elongation (%) | 26.4 | — |
| 70°F Charpy V-Notch (Ft. Lbs) | — | 46 |
| Trans. Temp. (°F) | — | 125 |
| Trans. Energy (Ft. Lbs) | — | 50 |



TESTED CASTING SHOWING STRESS COAT PATTERN

BREAKDOWN DATA

| | |
|-----------------------------------|------|
| Service Pressure (x1000 psi) | 0.6 |
| Yield Stress Pressure (x1000 psi) | 6.1 |
| Deformation Pressure (x1000 psi) | >90* |

*Substantial Deformation Was Not Yet Apparent When Equipment Limitations Halted The Test at 9000 psi

ASTM A781: The tension testing requirements of this specification are intended only to characterize the tensile properties of the heat for determination of conformance to the requirements of the applicable product specification. Such testing procedures are not intended to define the upper or lower limits of tensile properties at all possible test locations within a heat. It is well known and documented that tensile properties will vary within a heat or individual casting as a function of chemical composition, processing, testing procedure, and other factors. It is, therefore, incumbent on designers and engineers to use sound engineering judgement when using tension test results.

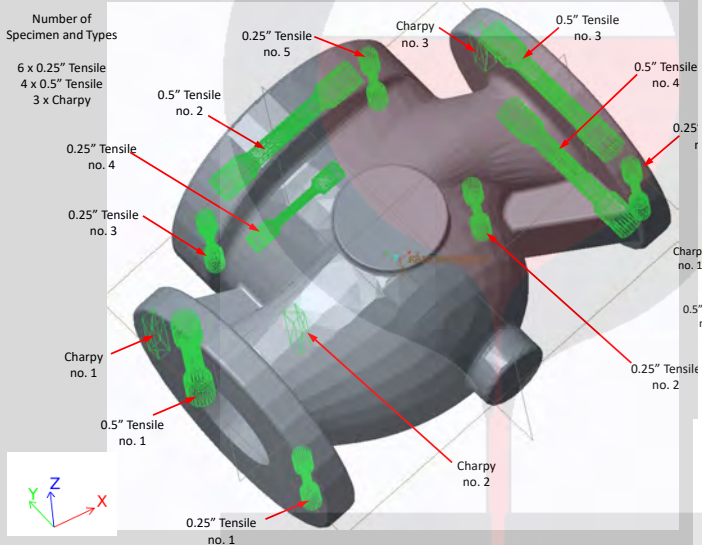


Commercial Casting Properties

Fitness for
service

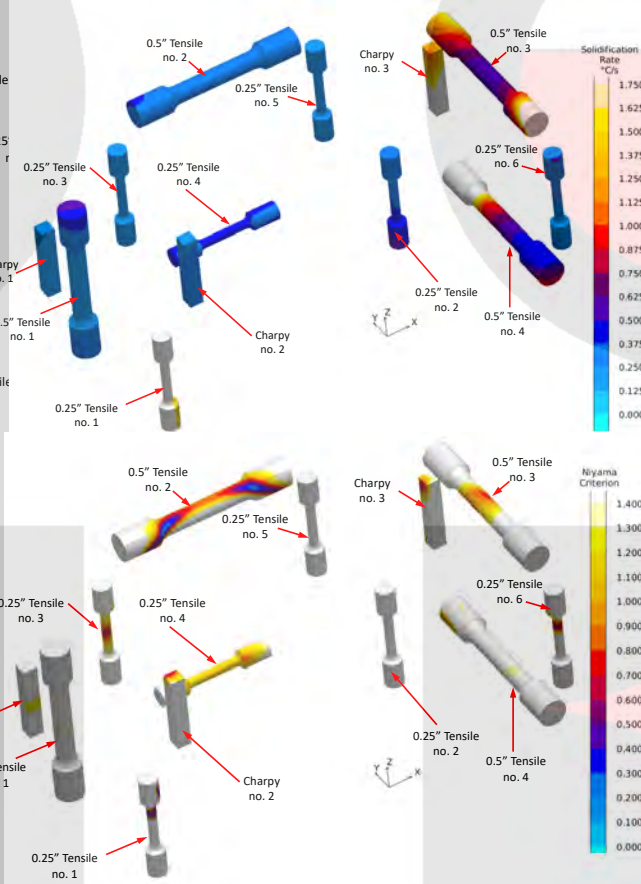
Number of
Specimen and Types

6 x 0.25" Tensile
4 x 0.5" Tensile
3 x Charpy



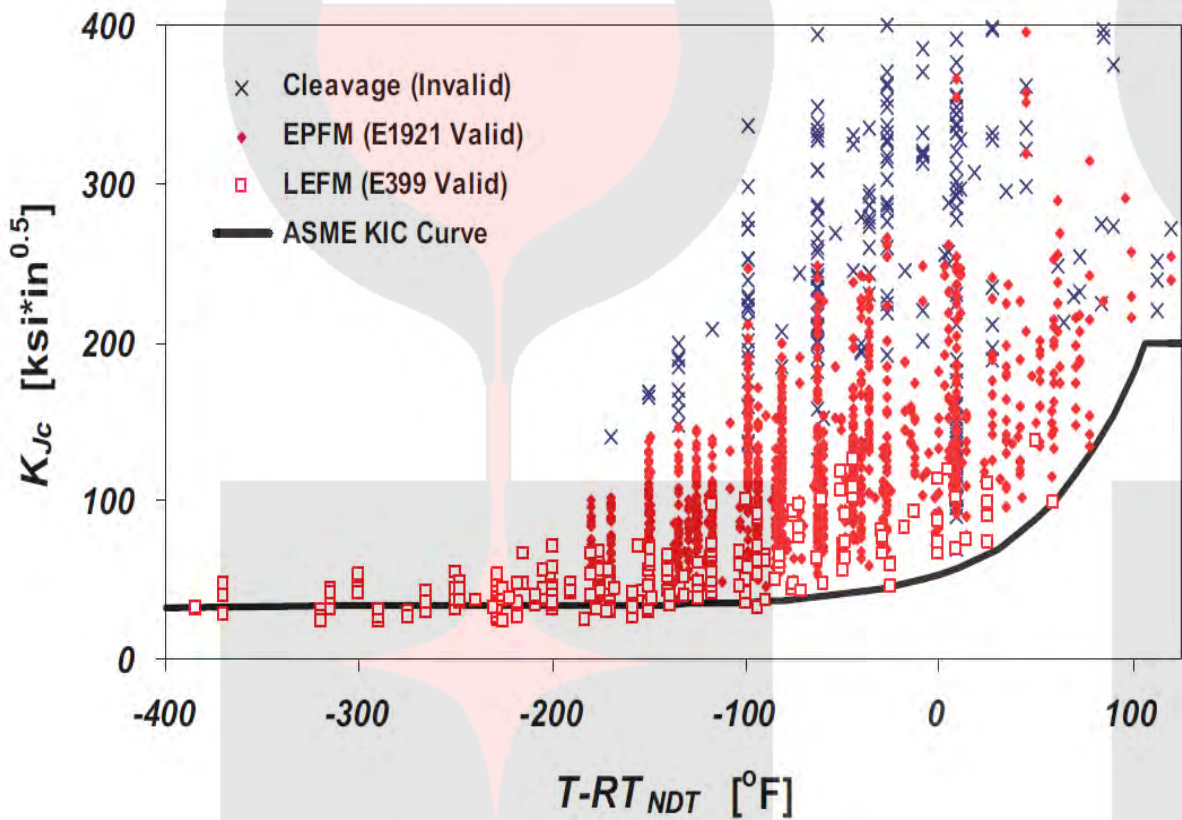
Modeling indicators

- Porosity
- Solidification rate (range and time)
- Niyama criterion
- Carbon segregation ratio
- Predicted properties
- Phase fractions of microstructures





Steel Master Curve

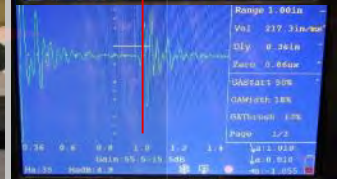
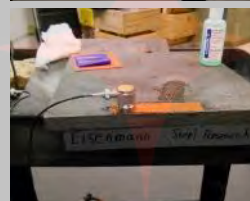
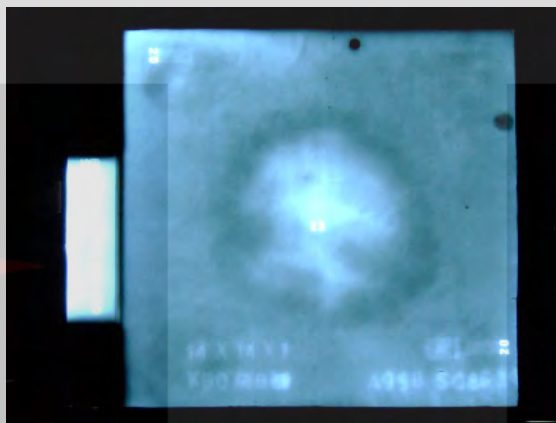
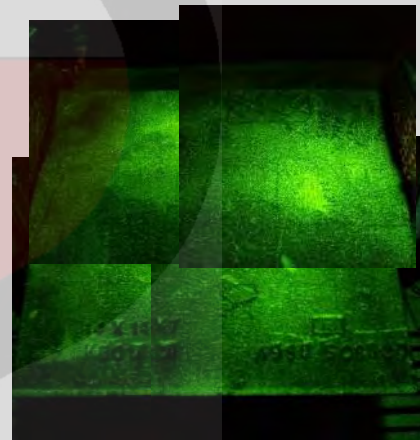
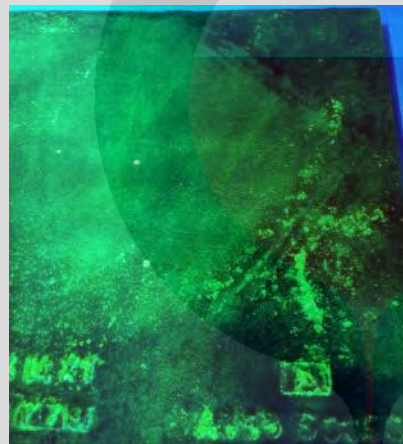


- Fracture toughness
- Based on Nil Ductility Temperature from CVN
- Conservative
- Cost-effective



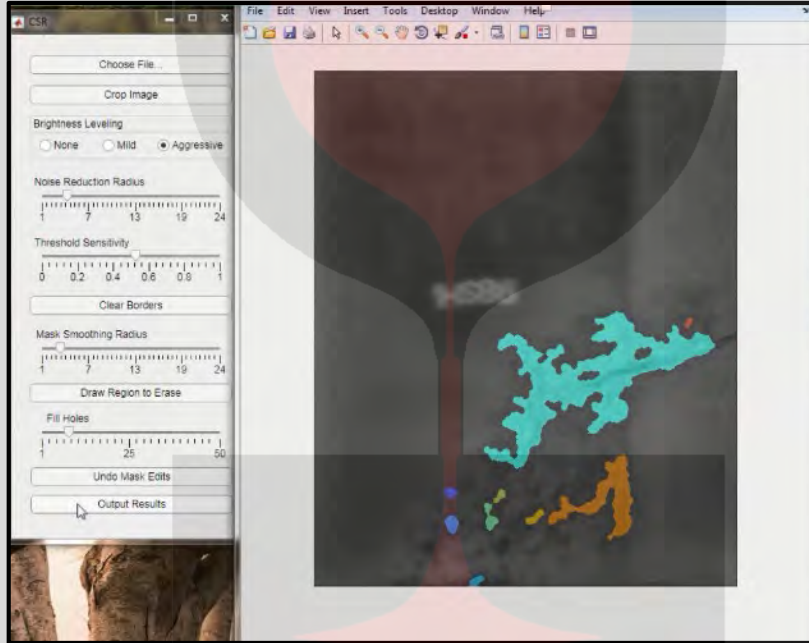
NDT Test Methods

- Visual
- Liquid penetrant
- Magnetic particle
- Radiographic
- Ultrasonic

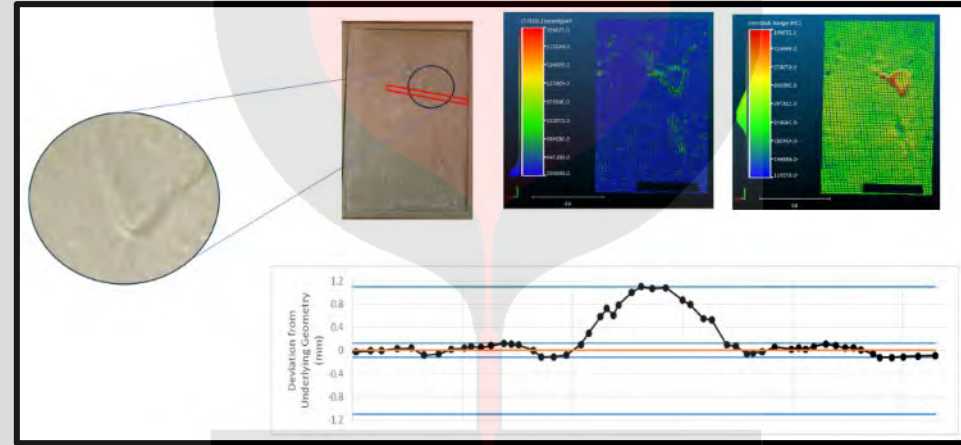




Quantitative NDT



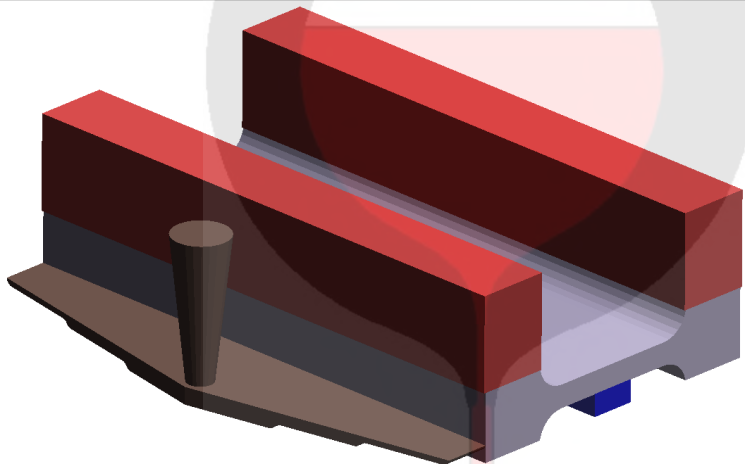
Automated image analysis (RT)



Digital surface inspection (visual)



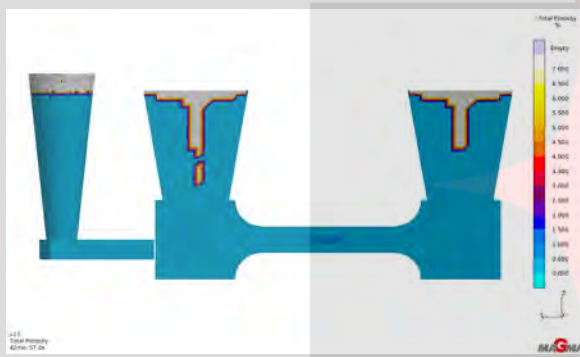
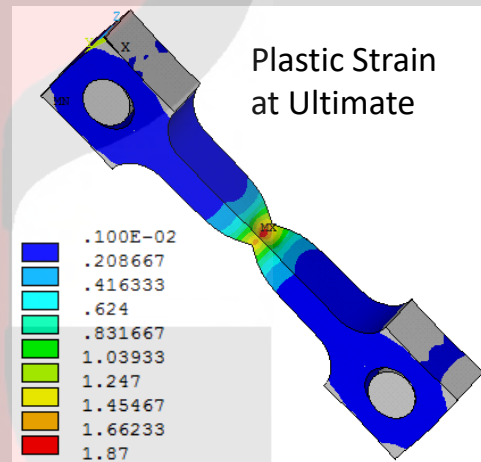
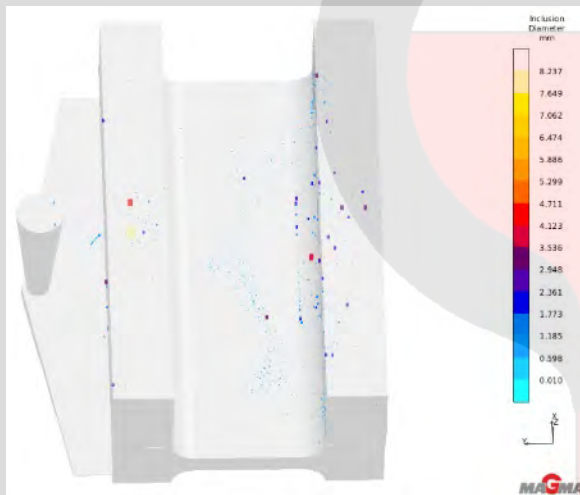
“Real” Test Specimens



Full Size Casting Test Demonstration

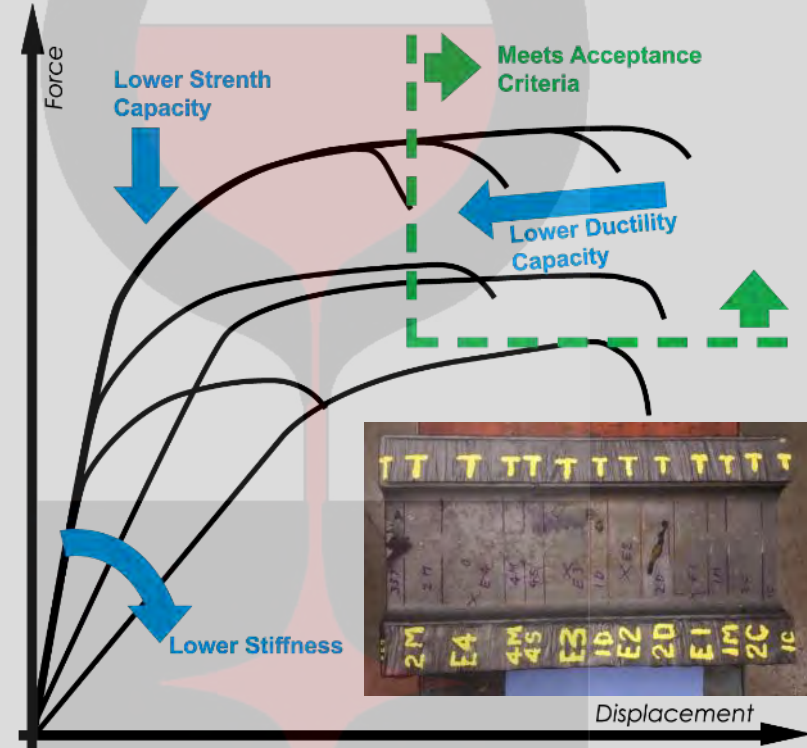
Casting Quality Effect on Performance:

- Surface finish
- Shrink Porosity
- Gas Porosity
- Inclusions



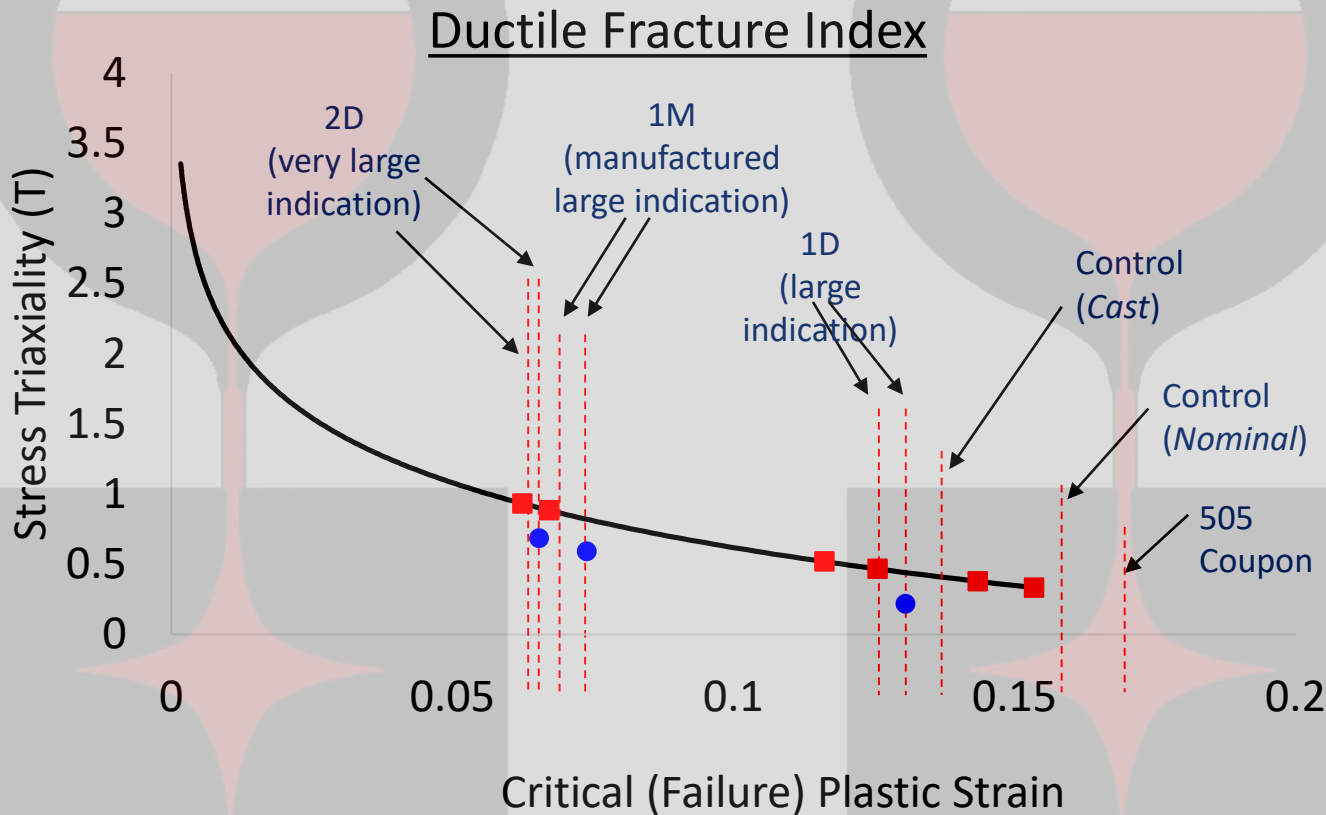


“Real” Test Specimens





“Real” Test Specimens



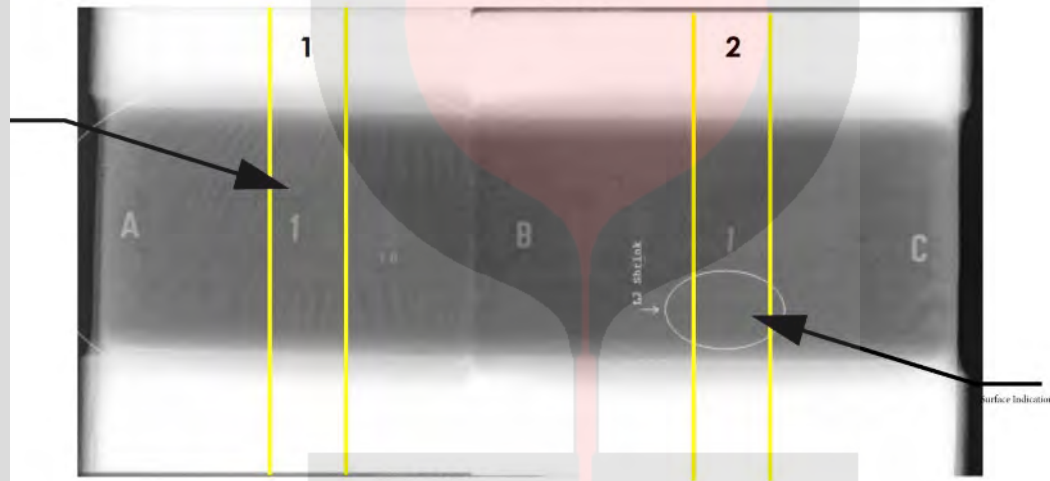


Phase I Castings: Internal Indications

Procedure

- Import radiograph into digital imaging software
- Convert Image into CMYK colors
- Establish baseline K value for grayscale intensity of solid regions
- Estimate location, size and depth of indications based on lower K values relative to baseline
- To ensure best possible modeling, average K value over the pixels in a given region were used for each indication

ing 1X



| | 1-1X-1 | | |
|----------------|--------|-------|-------|
| | | | |
| K Value | 79 | 26 | 30 |
| Thickness (in) | 0.000 | 1.076 | 0.995 |

| | 1-1X-2 | | |
|----------------|--------|-------|-------|
| | | | |
| K Value | 79 | 21 | 30 |
| Thickness (in) | 0.000 | 1.076 | 0.908 |

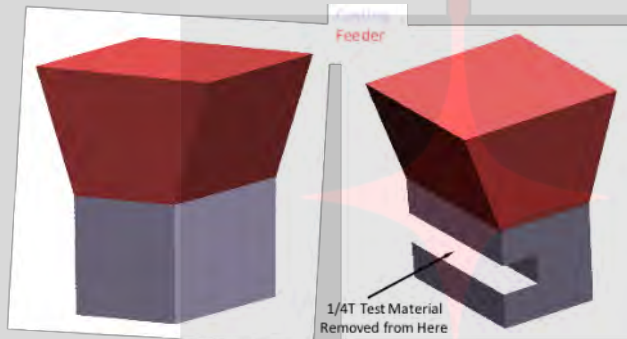
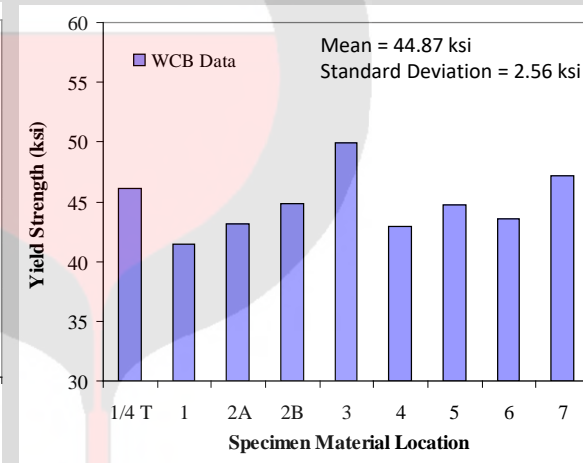
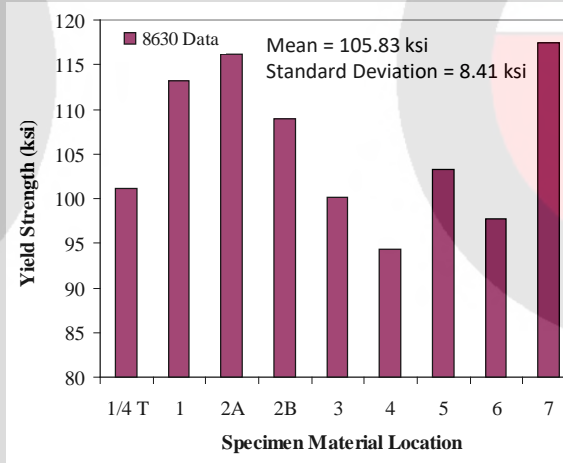


Heavy Section Mechanical Properties

Characterize mechanical properties and microstructure of heavy section castings

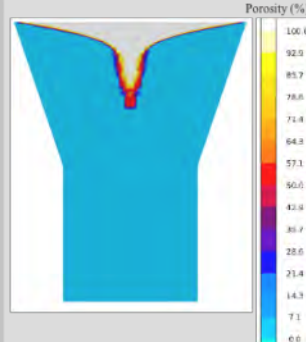
Preliminary analysis on:

- WCB and 8630
- 4" Y-blocks sectioned for tensile testing

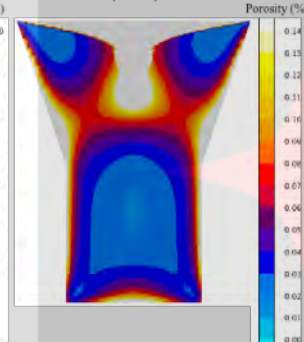


Default Boundary Condition Assumes Hot Topping and Good Feeding

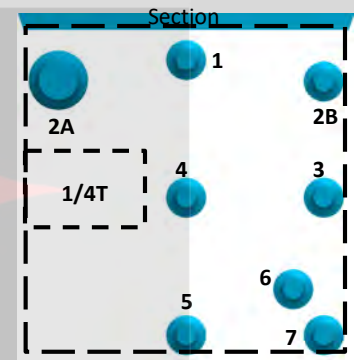
Full Porosity Scale



Microporosity Scale

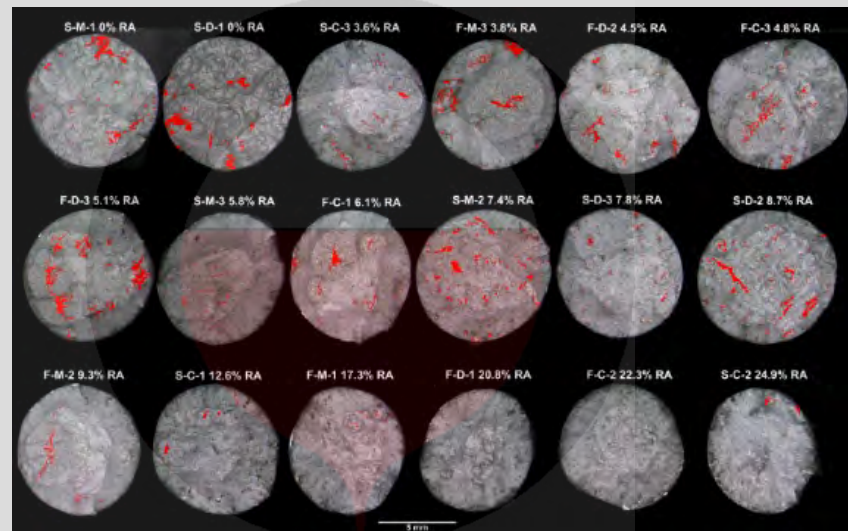
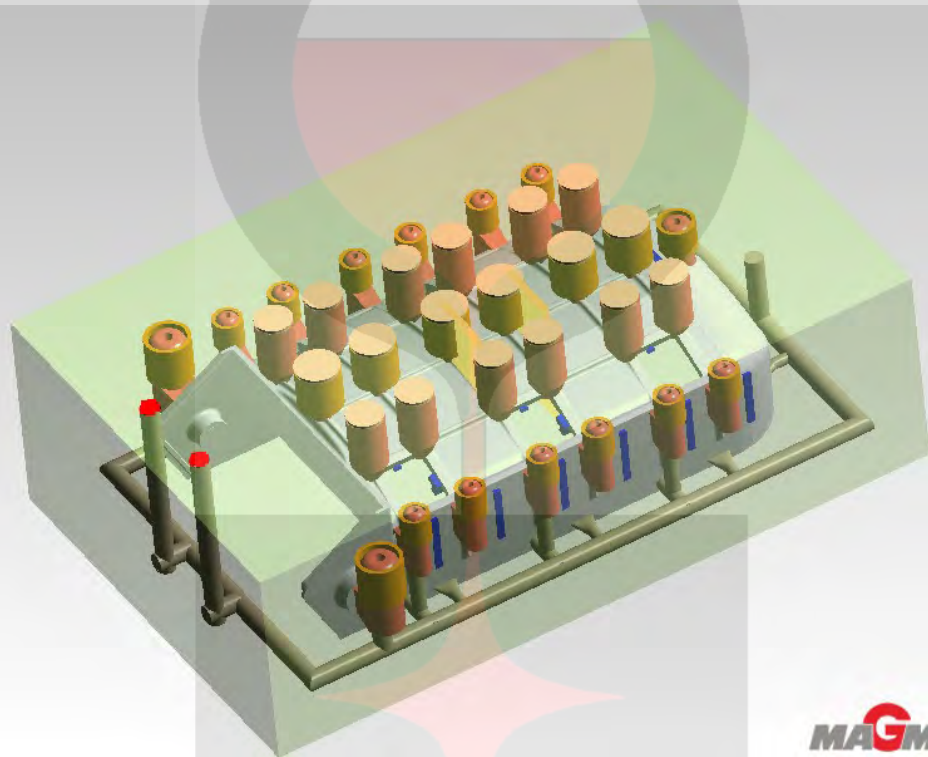


Numbering Scheme in Cross Section

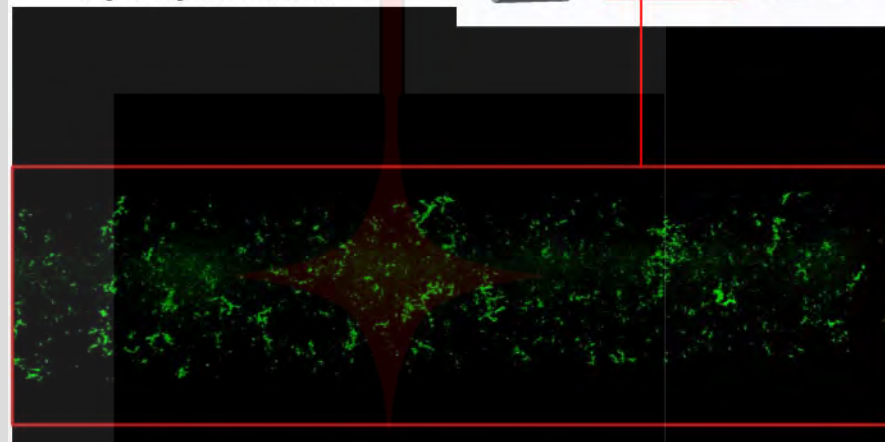




Max Pore Cluster Size



- Specimen diameter is 0.375" (9.53 mm)
Length of images below is about 1.5"



MAGMA



Production and Fabrication Welding

| | Alloy 1A | Alloy 1B | Alloy 2A | Alloy 2B |
|--------------|---------------|---------------|--------------------------|--------------------------|
| Cast-to-Cast | WCB | WCB | A148 Grade 115/95 (8630) | A148 Grade 115/95 (8630) |
| Cast-to-Mill | WCB | A516 Grade 70 | A148 Grade 115/95 (8630) | 4130 |
| Mill-to-Mill | A516 Grade 70 | A516 Grade 70 | 4130 | 4130 |

Alloy 1 – carbon steel

| Chemistry | C | Mn | Si | Cr | Ni | Mo | P | S | V | Cu |
|---------------|------|------|------|------|------|------|-------|-------|------|------|
| ASTM A216 WCB | 0.30 | 1.00 | 0.60 | 0.50 | 0.50 | 0.20 | 0.035 | 0.035 | 0.03 | 0.30 |
| Measured | 0.21 | 0.93 | 0.4 | 0.28 | 0.17 | 0.05 | 0.012 | 0.002 | 0.02 | 0.1 |



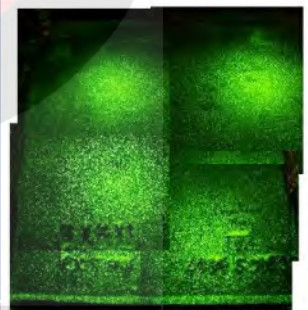
| | UTS, ksi | YS, ksi | %El | %RA |
|---------------|----------|---------|--------|--------|
| ASTM A216 WCB | 70-95 | 36 min | 22 min | 35 min |
| Measured* | 73 | 46 | 35 | 63 |

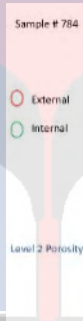
**1750F 4hrs, air cooled, 1200F 4hrs, air cooled*



Production and Fabrication Welding



| ASME BPVC Section IX (for $\frac{3}{4}'' \leq \text{test coupon } T < 1.5''$) ¹ | AWS D1.1 (for test coupon $T \geq 1''$) ² | Additional [Lehigh] Tests | ASTM A488 [Procedure] ($\frac{3}{4}''$ to $1\text{-}1/2''$ thickness) |
|--|---|---|---|
| 4 transverse side bend 2 reduced section tensile | 4 transverse side bend 2 reduced section tensile | 2 longitudinal root bend ³ 2 longitudinal face bend ³ 2 transverse root bend ⁴ 2 transverse face bend ⁴ 1 weld metal tensile ⁵ 1 macroetch ⁶ 1 macrohardness ⁷ CVN ⁸ | 4 transverse side bend 2 reduced section tensile |
|  |  | |  |



¹ Qualifies $3/16''$ to 2T base metal thickness

² Qualifies $3/16''$ and thicker

³ Required in ASME BPVC Section IX and AWS D1.1 only if bending properties between base metals or base metal and weld metal are markedly different (e.g. welding Grade 115 to Grade 60)

⁴ Required in ASME BPVC Section IX for test coupon $T < 3/4''$ and in AWS D1.1 for test coupon $T \leq 3/8''$

⁵ Required in AWS D1.1 to qualify ESW and EGW or to qualify filler metal (consumable)

⁶ Required in AWS D1.1 for PJP and fillet welds

⁷ For informational purposes only

⁸ CVN is not required by the material specification A148 115/95 so CVN test will be done only for informational purposes. CVN test will be @ lower shelf temperature (to be determined from DBTT testing of cast base metal). Lower shelf T is typically used because it is the worst case scenario (provides most conservative value). **Test at 2 locations (3 samples each location): weld metal and HAZ (on cast-to-mill, HAZ in both sides will be tested)**



Summary of Results (as per D1.1)

Charpy Impact Testing is underway



| Test Type | Direction | Number of Tests | Cast to Cast (A216 WCB to A216 WCB) | Cast to Wrought (A216WCB to A516 Grade70) | Wrought to Wrought (A516 Grade70 to A516 Grade70) |
|--------------|-------------------|-----------------|--|---|--|
| Bend Test | Transverse Root | 2 | Acceptable | Acceptable (note: 2-retests) (Initial 1 of 2 unacceptable) | Acceptable |
| | Transverse Face | 2 | Acceptable | Acceptable | Acceptable |
| | Longitudinal Face | 2 | Acceptable | Acceptable (note: 2-retests) (Initial 1 of 2 unacceptable) | Acceptable |
| | Longitudinal Root | 2 | Acceptable | Acceptable | Acceptable |
| | Transverse Side | 4 | Acceptable | Acceptable | Acceptable |
| Tensile Test | Transverse | 2 | Avg. UTS: 73.8 ksi Failure Location: Base Metal | Avg. UTS: 75 ksi Failure Location: Base Metal | Avg. UTS: 79.3 ksi Failure Location: Base Metal |
| | All Weld | 1 | YS: 90.5 ksi UTS: 97.6 ksi %Elongation: 24 | YS: 87 ksi UTS: 94.8 ksi %Elongation: 24 | YS: 75.5 ksi UTS: 86.3 ksi %Elongation: 27 |
| | Base Metal | 2 | YS: 38.4 ksi UTS: 72.8 ksi %Elongation: 29 | none | YS: 47.5 ksi UTS: 78.1 ksi %Elongation: 34 |



Design Resources

<https://www.sfsa.org/publications/>

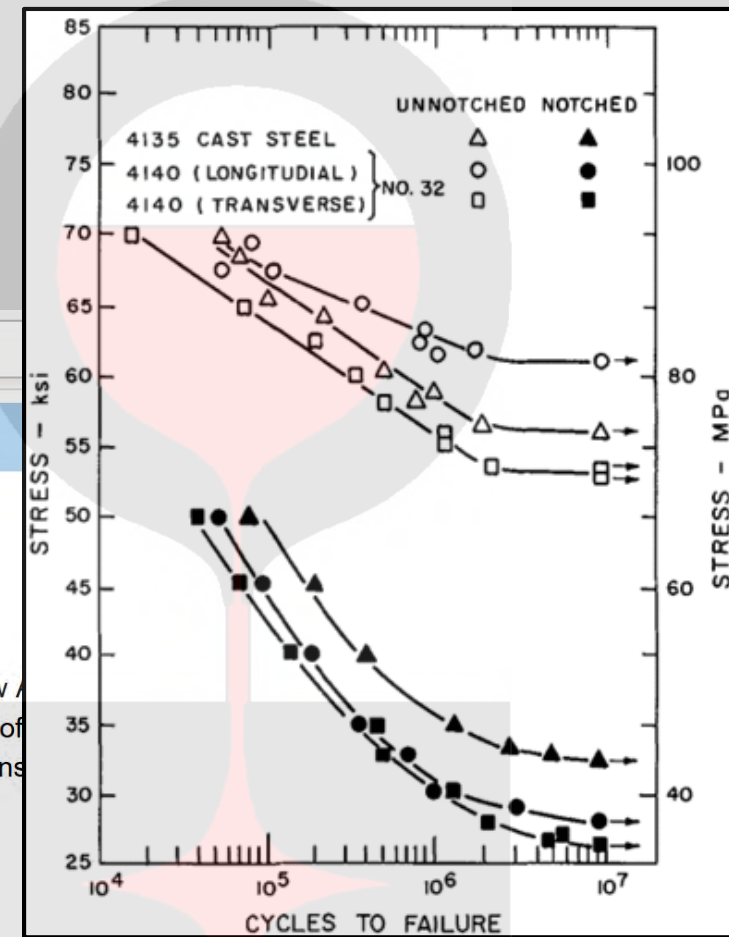
Free publications

Casteel Reporter - SFSA's newsletter

Other free SFSA publications:

- Supplements to the Steel Castings Handbook
- **Research Reports 94 A&B** on Fatigue and Fracture Toughness of Five Carbon or Low Alloy Steel Castings
- **SFSA Project A95** on Corrosion, Toughness, Weldability and Metallurgical Evaluation of Steel Castings
- **Test Coupons and Casting Properties** Information gathered from several publications on test coupons and the properties of castings
- **Fracture Toughness in Relation to Steel Castings Design and Application**
- Ultrasonic Testing of Steel Castings
- Cast to Shape. A history of the steel castings industry in the United States
- Raw Materials Specifications
- Sub-size Charpy specimens

<http://user.engineering.uiowa.edu/~becker/documents.dir/SFSA/2003-3.5%20Fatigue%20of%208630.pdf>





Questions

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Real casting properties
Test specimens v. real castings
Welding – minor v. major
Design/customers